

3-D Seamless Knitted Preforms for Automotive Seating Applications

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seating
door trims
headliners
floor carpets
nvh products
spoilers
aftermarket



HOLDEN



VE SWB



WM LWB



HSV sports



Utility



Wagon

seating
steering
pedals
window regs
headliners
floor carpets
nvh products
aftermarket



SWB sedan



FPV sports



Utility



Wagon



Territory
SUV

headliners
nvh products
spoilers
aftermarket



Camry &
Aurion

aftermarket
& vehicle
personalisation



products
vehicle



electronics
vehicle security
driver aids
vehicle safety
aids



rear-seat
entertainment
packaging
carpet floor mats





A21



S21



M12



M11



M14



B21



A01



plus other confidential



A108



B926



Elfin (Aust export)



Comparison of various textile preforms



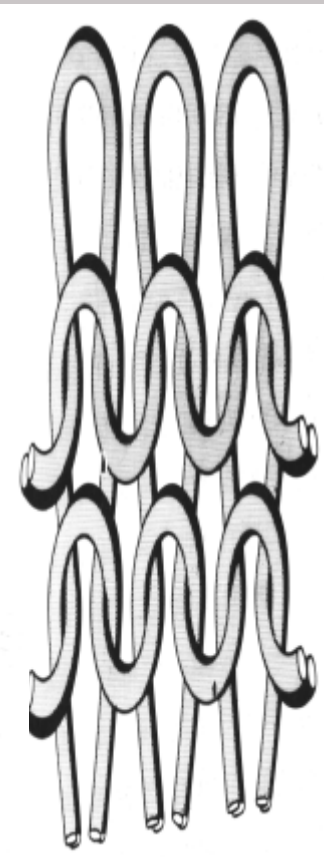
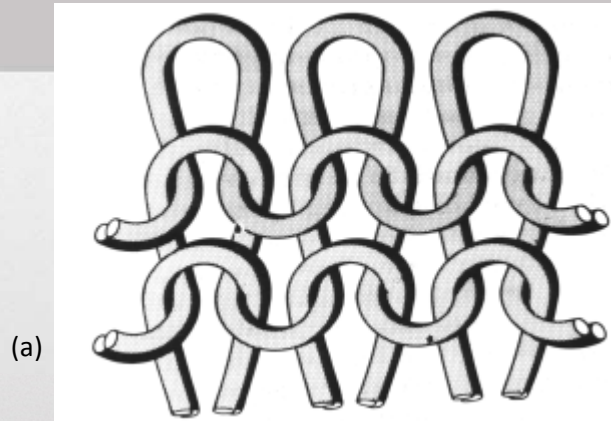
In order of best to worst for each parameter

<i>Strength & Modulus</i>	<i>Cost</i>	<i>Damage Tolerance</i>	<i>Formability</i>	<i>Waste</i>
UD Tape	Non woven	Knitted	Knitted	Knitted
NCF	Knitted	Nonwoven	Nonwoven	Nonwoven
Braid	Woven	Braid	UD Tape	Braid
Woven	UD Tape	UD Tape	Woven	UD Tape
Knitted	NCF	Woven	NCF	Woven
Non woven	Braid	NCF	Braid	NCF

Knitted preforms – Effects of yarn orientation



Single jersey
un-stretched



Single jersey
wale-stretched

Single jersey
course-
stretched

Strength and stiffness increases in the direction of stretch at the expense of the orthogonal direction

Effects of Fibre Orientation - Nonwoven



(a) No Stretch



(b) 75% MD Stretch



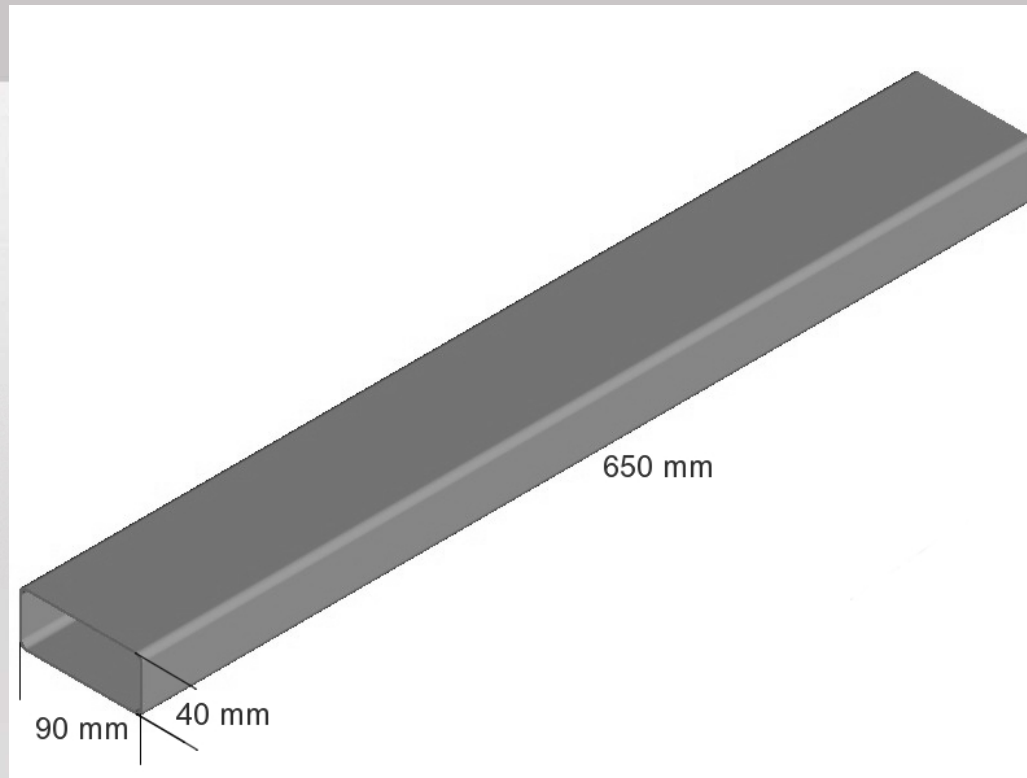
(c) 100% MD Stretch

Nonwoven Twaron fabric has ~ 4:1 MD:CD orientation and fibres are highly crimped. Stretching in the MD gives straighter fibres and aligns them in the machine direction to give higher strength and stiffness



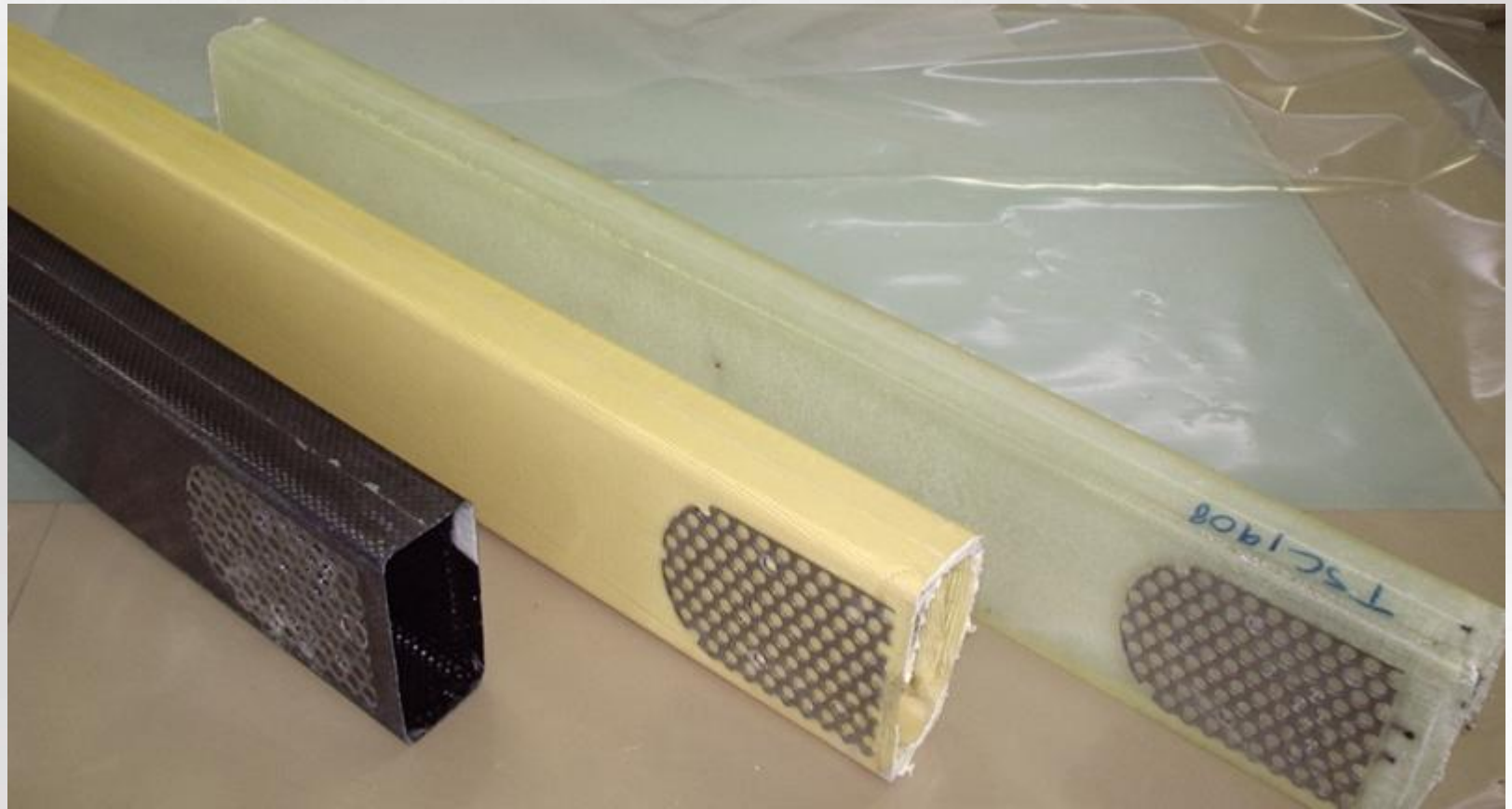
Effects of Orientation

Fabric Type & Conditions	Test direction	Ultimate Tensile strength (MPa)	Axial strain (%)	E Modulus (GPa)
Non-Wovens				
Epoxy – Twaron (cured 80C/12min)	MD	51	1.8%	3.00
Twaron stretched along MD	MD	122	2.1%	6.00
Twaron stretched along MD	CD	93	2.1%	5.50
Knitted				
Epoxy Twaron-No stretch	Whale	137	11.0%	7.67
Twaron 75% stretch along courses	Whale	157	6.9%	7.67
Twaron 100% stretch along courses	Whale	196	8.5%	9.00
R246 (cold cure) Twaron Knit Stretch-MD 1	MD	201	2.7%	9.89
	CD	45	3.7%	3.55
Twaron-R246 Knit Stretch-MD 2	MD	182	6%	15.1
	CD	38	4%	4.5
Twaron-R246 Knit Stretch-CD	MD	55	2.6%	5.1
	CD	75	5%	6.6



**Test beam dimensions.
The wall thickness varied but
was usually approximately 2 mm.**

Carbon, Aramid, and glass fibre beams





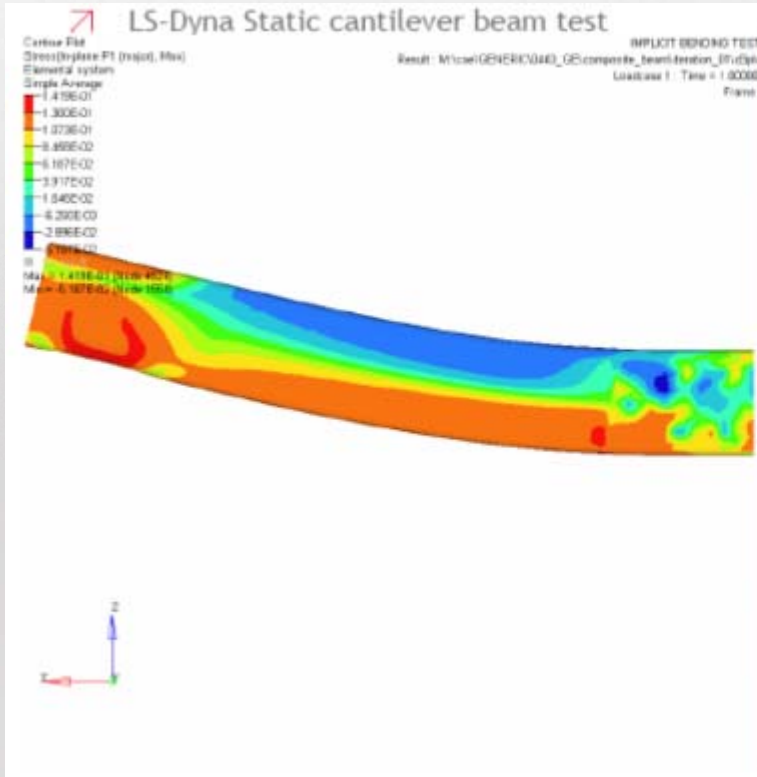
Hot press and beam mould



Shima Seiki 3D Whole-Garment knitting machine, 14G

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Beam Testing Results



	Transition Values - maximum elastic limit of material			Ultimate values - for max stress/strain ¹		
	Value	Unit	Stdev	Value	Unit	Stdev
In-Plane Tensile Test						
E11 Modulus longitudinal	8.48	GPa	0.72	8.48	GPa	0.72
E22 Modulus transverse	4.83	GPa	0.73	4.83	GPa	0.73
Poisson's Ratio ₁₂ - Poisson ratio in the 1-2 direction	0.55		0.088	0.55		0.088
σ_{11} UTS longitudinal	75.1	MPa	4.9	99.7	MPa	8.1
σ_{12} UTS transverse	30	MPa	1.3	35.7	MPa	1.1
ϵ_{11} TFS longitudinal	0.0135		8E-04	0.05		0.018
ϵ_{12} TFS transverse	0.0082		5E-04	0.02		0.002
In-Plane Compression Test						
E11 Modulus longitudinal	1.67	GPa	0.44	1.67	GPa	0.44
E22 Modulus transverse	1.82	GPa	0.45	1.82	GPa	0.45
σ_{11} UCS longitudinal	51.9	MPa	2.8	64.9	MPa	2.8
σ_{12} UCS transverse	55.8	MPa	2	69.8	MPa	2
ϵ_{11} CFS longitudinal	0.0458		0.01	0.08		0.013
ϵ_{12} CFS transverse	0.0418		0.008	0.08		0.021
In-Plane Shear Tests						
G ₁₂ shear modulus in the 1-2 direction	2.18	GPa	0.04	2.18	GPa	0.04
G ₂₃ shear modulus in the 2-3 direction	1.4	GPa	0.01	1.4	GPa	0.01
G ₃₁ shear modulus in the 3-1 direction	1.31	GPa	0.01	1.31	GPa	0.01
T ultimate shear strength in the 1-2 plane	38.5	MPa	2.13	42.8	MPa	2.13
Y shear failure strain	0.0206		0.002	0.03		0.002
Through Thickness Compression Test						
E ₃₃ through thickness modulus	1.79	GPa	0.33	1.79	GPa	0.33

¹Strain at maximum stress rather than ultimate failure is given.

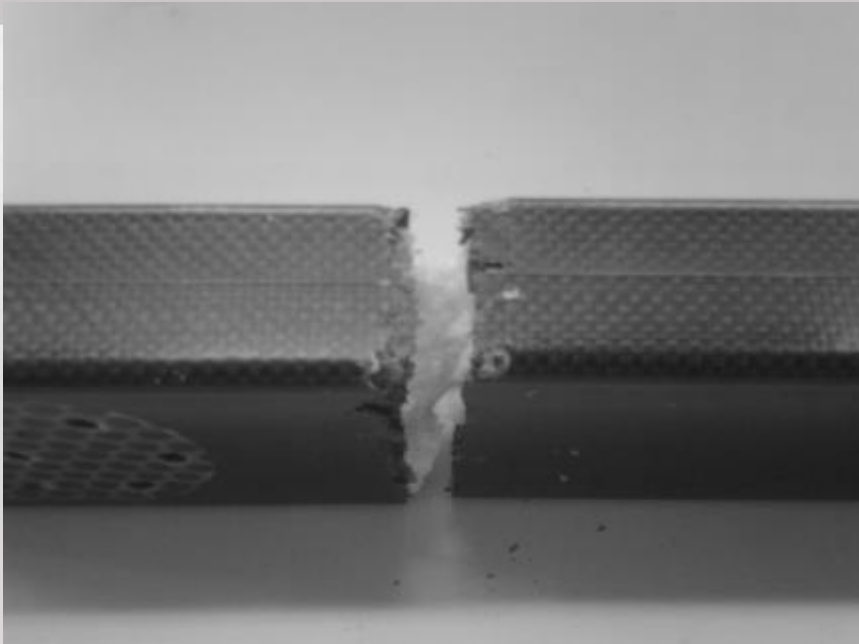
²Not the strongest material produced but one used for model verification

Summary of Beam Tests



Beam Type	Beam Mass (g)	Mass per Lineal Metre (kg/m)	Failure Torque (Nm)	Specific strength (Nm ² /kg)
Steel (0.9mm wall)	1200	2.00	1668	910
Aramid Rib + local woven aramid	617	0.82	1295	1582
Woven Glass (5 layers)	514	0.66	980	1497
Woven Carbon (5 layers)	509	0.70	2326	3318
Woven Aramid (2 layers)	365	0.48	564	1166
Aramid Jersey Knit	481	0.68	973	1437
Aramid Jersey Knit + spacer (small size)	492	0.75	1225	1654
2 Layer Aramid Rib	749	1.21	1936	1624
2 Layer Aramid Rib + local reinforcement	573	0.83	1588	1927
Single Layer Aramid Rib	489	0.72	613	849
Longitudinal courses Knit	508	0.76	1247	1646
Warp insertion weft knit (0/90 combined)	506	0.76	1301	1706
Hybrid Nylon / woven carbon beam	560	0.84	1323	1566
4 layer Twaron (2x folded 510 circumference)	510	0.76	931	1227
Hybrid with straight yarns	533	0.88	1567	1764

Beam test results



Woven carbon Beam



Knitted Twaron Beam

Woven Carbon fibre produced the stiffest, strongest beams but wovens cannot be easily formed into 3d shapes. Carbon also cannot be easily knitted and its failure mode is to fracture leaving sharp edges. Hybrids show promise but add complexity to manufacturing. Knitted preforms fail in a more benign manner that increases occupant safety in an accident.

Infusion Studies, effect of pressure difference



Nylon17 (above) full vacuum – 103KPa



Nylon18 (above) half vacuum – 50KPa



Nylon19 (above) quarter vacuum – 25KPa

Knits can provide excellent infusion rates, yarns and knit structures affect rates

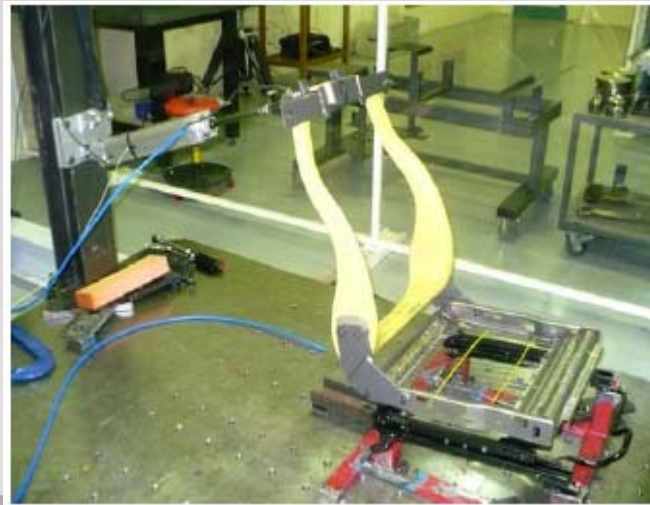
First Prototype aramid composite seat frame





Rearward static load

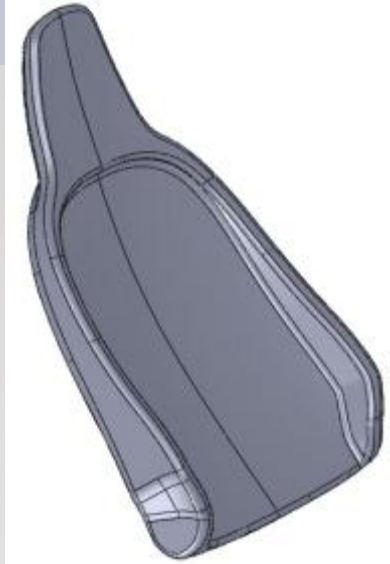
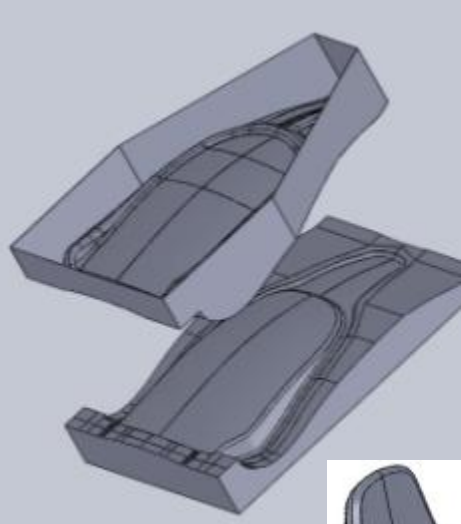
Average Load	Load (kN)	Torque (Nm)
Composite	3.47	2061
Steel	3.31	1806



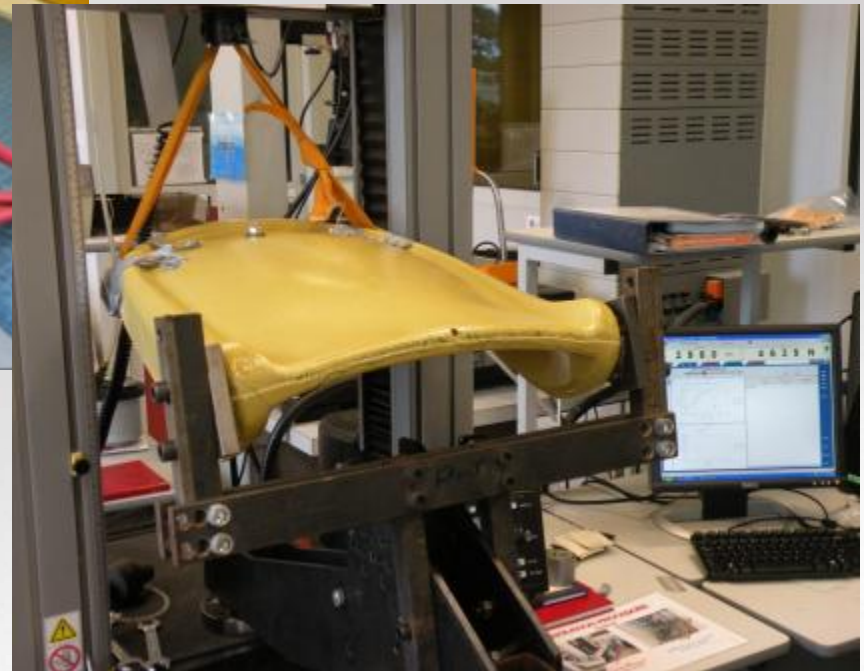
Durability test

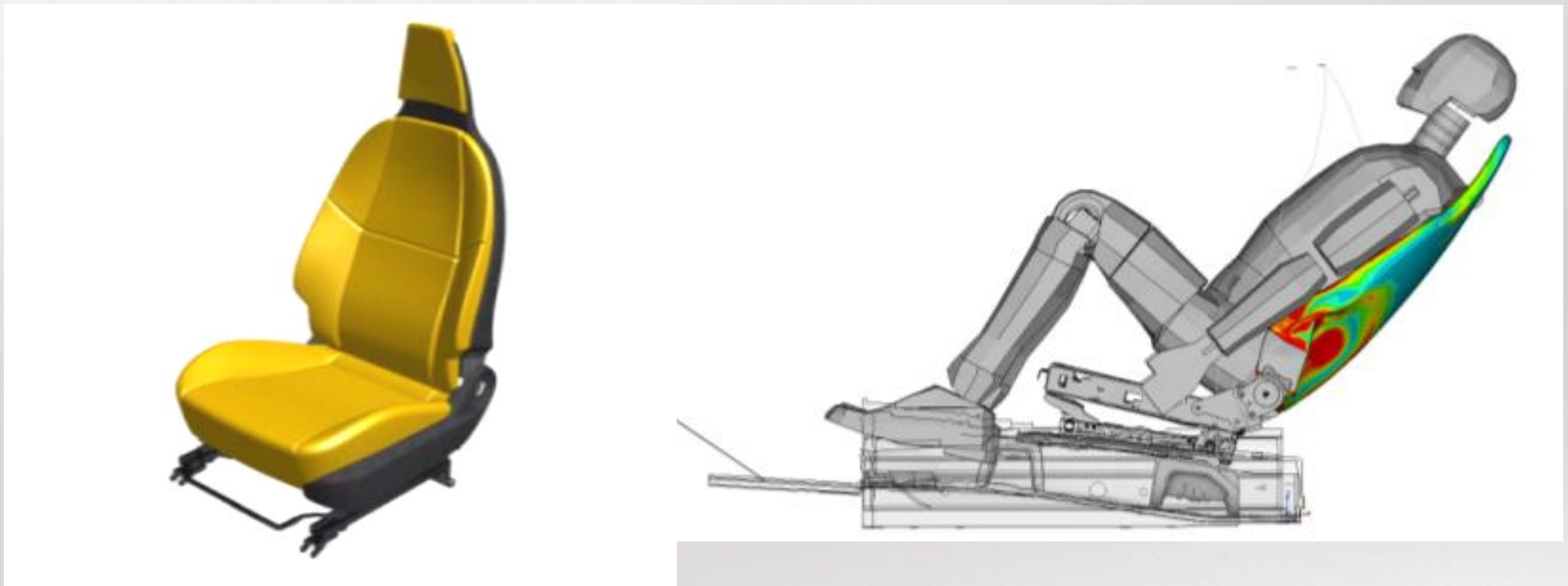
50,000 fatigue cycles -
passed

Second Prototype Design: Monocoque Seat mould



Clam-shell mould and destructive testing





The final design was shown to pass most of the industry requirements and was lighter than existing seats while being price competitive

3D knitted structure – benefits over existing steel frame



Reduce weight, time to market, and cost

- Utilise CAE technology – design optimisation & validation
- Eliminate labour intensive lay-up processes
- Eliminate tooling, heavy presses, welding
- Integrate features, form and function
- Manufacture close to the end user
- Minimise waste



Design flexibility with customisation potential

- Quick design changes possible
- CAD to preform in short time
- Low cost tooling
- Rapid manufacturing methods
- Prototype to production with more confidence

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The logo for Futuris, with the word "FUTURiS" in a bold, italicized font. "FUTUR" is in black and "iS" is in red.